Thermal analysis of solid and vented disc brake during the braking process

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Abstract

Braking system is one of the most important components of a vehicle on the road. This system has the task to bring the vehicle to stop or slow down. Friction brakes, during the braking process, convert the kinetic and potential energy into the thermal energy (heat). The basic components of braking systems, brake discs and brake pads, in a short period of time absorb a large amount of heat release (Travaglia et al. 2014). The absorbed heat must be, as far as possible, effectively dissipated in order to ensure the normal operation of the braking system (Day et al. 1984). High temperature during the braking process may cause many problems such as thermal cracks, premature wear, brake fade and thermally-excited vibration (Lee 1999). In this study, a typical disc brake system was modeled including brake disc and pads. Using COMSOL Multiphysics 5.0, we investigated thermal behavior of two types of discs – solid and vented discs. The results show that the vented disc is a much better solution than the solid disc, because the greater amount of heat is released for the same amount of time.

Keywords: Brake disc, thermal analysis, heat dissipation, COMSOL Multiphysics 5.0

1. Introduction

As is well known, the braking system is used to bring the vehicle to stop or slow down. The kinetic energy of the vehicle is transformed into the thermal energy. Brake discs and brake pads absorb the largest part of this energy and, after that, this energy is dissipated into the surrounding (Talati et al. 2009). Currently, more than 2000 materials and their variants are used in the manufacture of brake components. A brake disc is usually made of cast iron or ceramic composites, while a brake pad is made from frictional material. During the braking process, the temperature, as a result of friction between a brake disc and disc pads, can have values in the range of 200 to 800 °C (Idusuyi et al. 2014). Heat generation is a function of vehicle mass, friction coefficient, thermo physical properties of material, velocity and rate of deceleration. Heat dissipation will occur via:

• conduction through the brake assembly,
• radiation to nearby components and
• convection to the atmosphere.

Heat dissipation through conduction on nearby components can lead to damaged seals, brake fluid vaporization, or wheel bearing damage. The total amount of heat dissipation through
radiation is less than 5% of total heat dissipation (Limpert 1975). The most important heat
dissipation occurs by convection to the atmosphere. Using Newton’s law of cooling, convection
can be expressed as:

\[ Q = hA_s (T_s - T_\infty) \]  

Where \( Q \) is the rate of heat transfer, \( h \) the convection coefficient, \( A_s \) the surface area of
the disc, \( T_s \) surface temperature and \( T_\infty \) is ambient air temperature. In order to maximize heat
transfer from a brake disc, and keep disc temperature to a minimum, surface area \( A_s \) or value of
convection coefficient \( h \) needs to be increased. Using a vented brake disc will increase the
surface area because there is an additional surface area exposed to atmosphere which will lead to
a better cooling (Belhocine et al. 2014).

Finite element method gives a possibility to analyze heat conduction in disc brake system.
Our task was to study the heat generation and dissipation in a disc brake during a panic car
braking for two seconds and following a release period of six seconds using COMSOL
Multiphysics 5.0. The car (1600 kg) initially travels at 90 km/h. Suddenly, the driver hits the
brakes for two seconds, and then releases the brakes for 6 seconds. The wheels are assumed not
to skid against the road surface. Using 3D simulation, we have observed temperature changes on
the brake disc during the braking and the cooling process after braking.

2. Materials and methods

2.1 Governing equations

The kinetic energy of the vehicle in motion can be expressed as:

\[ E = \frac{1}{2} m (v_1^2 - v_2^2) \]  

where \( m \) is vehicle mass, \( v_1 \) initial velocity and \( v_2 \) is reduced velocity. If we neglect drag
and other losses, the brakes retardation power is equal to the negative derivative of kinetic energy
(Petinrin et al. 2012):

\[ P = -\frac{d}{dt} \left( \frac{mv^2}{2} \right) = -m v \frac{dv}{dt} = -m R^2 \omega(t) \alpha \]  

where \( m \) is vehicle mass, \( R \) is wheel radius, \( \omega \) is angular velocity, and \( \alpha \) is the angular
acceleration.

The friction force per unit area, \( f_f \) is approximately constant over the surface area of eight
pads (two pads per brake disc) and is directed opposite the brake disc velocity vector:

\[ P = -8 \iiint f_f dA \cdot v_d = -8 f_f (t) \omega(t) \iiint r dA \]  

Using the previous two equations, the frictional force can be determined as:

\[ f_f = -\frac{m R^2 \alpha}{8 r_m A} \]
where \( r_m \) is the distance between the center of the brake disc and the pad center of mass, and \( \alpha \) is negative acceleration during retardation.

The heat power generated on the contact area can be defined as:

\[
q(r,t) = -f_\text{r} \cdot v(r,t) = -\frac{mR^2 \alpha}{8r_m A} r(\omega_0 + \alpha t)
\]  

(6)

The heat dissipation from the brake disc and pad surfaces to the surrounding air is described by convection and radiation as:

\[
q_{\text{diss}} = -h(T - T_{\text{ref}}) - \varepsilon \sigma (T^4 - T_{\text{ref}}^4)
\]  

(7)

where \( h \) is convective film coefficient, \( \varepsilon \) is the material emissivity, and \( \sigma \) is the Stefan-Boltzmann constant.

2.2 Model definition

The model of the complete disc brake is generated using Catia v5 R18 software. The model of the full brake disc with the main dimensions is shown in Fig. 1.

![Fig. 1. 3D model of brake disc and brake pads (solid and vented disc)](image)

Meshing of the brake disc and brake pads has been done using Comsol Multiphysics 5.0. The complete mesh of the full disc consists of 77626 tetrahedral elements, while the complete mesh of the vented disc consists of 95341 tetrahedral elements.

The mass of the vehicle used for analysis is 1600 kg. The initial velocity is 90 km/h. Suddenly, the driver hits the brakes for two seconds, causing the vehicle to slow down at a rate of 10 m/s\(^2\), and then releases the brakes for 6 seconds. Fig. 2 shows the change in vehicle velocity during the braking process.
Brake discs are commonly manufactured of cast iron. This material has good thermo-physical characteristics. The material of brake pad is asbestos. Their material properties are given in Table 1.

<table>
<thead>
<tr>
<th>Material properties</th>
<th>Cast iron</th>
<th>Asbestos</th>
</tr>
</thead>
<tbody>
<tr>
<td>Density [kg/m$^3$]</td>
<td>7870</td>
<td>2000</td>
</tr>
<tr>
<td>Heat capacity [J/(kgK)]</td>
<td>449</td>
<td>935</td>
</tr>
<tr>
<td>Thermal conductivity [W/(mK)]</td>
<td>72</td>
<td>8.7</td>
</tr>
</tbody>
</table>

**Table 1.** Material properties of brake disc and pad

3. Results and discussion

The 3D finite element analysis of the temperature of the brake disc during the braking was done using COMSOL Multiphysics 5.0. We used Heat transfer in solids module. Fig. 3 shows the temperature distribution for the full brake disc at different time steps.
The beginning of the braking process is characterized by temperatures of 72 °C in contact brake disc and pads. As the process of braking continues, the temperature rises quickly and reaches a maximum value of 182 °C. In addition, with this simulation we wanted to show how the brake disc cools after completing the braking. The temperature distribution at that point in time is shown in Fig. 3d. Fig. 4 shows the temperature distribution for the vented disc at four different time steps.
The previous figure visually shows that the vented disc is less heated than the solid disc. Maximum temperature that is released in this process of braking is 166 °C (Fig. 4b). After releasing the brakes, after 6 seconds, the maximum value of temperature is 118 °C, which is substantially less than in the case of the solid disc. The reason for that is the space between the vanes, which increases heat dissipation from the disc.

Fig. 5 shows the variation of temperature versus time during the braking process for solid and vented brake disc. The highest temperature occurs approximately 1 s after engaging the brake in the contact surface of the brake disc and the pads. At time t = 4s (end of braking), a maximum temperature of 157.9 °C is achieved on the solid disc. For the same time interval, the vented disc generates a temperature of 147.5 °C. It may be noted that the vented disc is a better solution because the heat is much better drained from its surface. Vanes geometry and their total number greatly affects the heat dissipation from the brake disc.

4. Conclusions

The previous section shows the research results of the thermal behavior of parts of the brake system during vehicle stops. Numerical simulations of the thermal behavior of a solid and ventilated disc were done using COMSOL Multiphysics 5.0. For the given braking conditions, the highest temperature that was generated on the solid disc was 182 °C, while the ventilated disc heated to 166 °C. Comparing the different results obtained from the analysis, it can be concluded
that the ventilated brake disc is a better solution, because it contains additional surfaces from which the heat dissipates. Disc brake design plays an important role in heat transfer. It would be interesting to see how the temperature distribution is influenced by various forms of vanes and their thickness. Our future research will go in that direction.

Извод

Термална анализа чврстог и вентилирајућег диска током процеса кочења

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Резиме

Кочиони систем је један од најважнијих компоненти возила на путу. Овај систем има задатак да заустави возило или да га успори. Фрикционе кочнице, током процеса кочења, претварају кинетичку и потенцијалну енергију у термалну енергију (топлоту). Основне компоненте кочионих система, кочиони дискови и кочионе плочице, у кратком временском периоду апсорбују велику количину ослобођене топлоте (Travaglia et al. 2014). Апсорбована топлота мора бити, колико је могуће, ефикасно расута како би се осигурао нормалан рад система за кочење (Day et al. 1984). Висока температура током кочења може изазвати многе проблеме као што су термалне пукотине, прерано хабање, затим кочнице бледе и могућа је појава термичких вибрација (Lee 1999). У овом истраживању, моделиран је типичан кочиони систем који укључује кочиони диск и кочионе плочице. Користећи COMSOL Multiphysics 5.0, истражено је топлотно понашање две врсте дискова: чврстих - солид и вентилирајућих. Резултати показују да је вентилирајући диск много боље решење од чврстих дискова, јер се доста већа количина топлоте ослобађа са вентилирајућег диска за исто време.

Кључне речи: Кочиони диск, топлотна анализа, дисипација топлоте, COMSOL Multiphysics 5.0.

References

